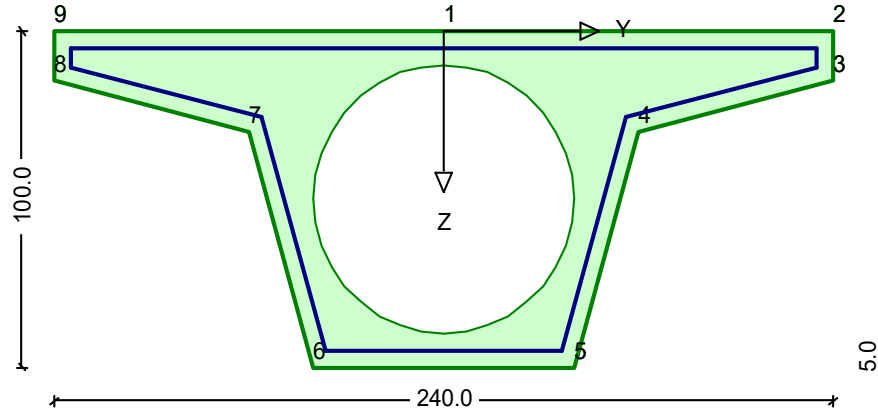


## Footbridge

File: Fußgängersteg.zwv



Bereich: Footbridge Design with  $A_s' < A_s$ , Querschnitt: Web Cross-Section

RIB ZWAX 18.0 Biaxial bending with normal force

Footbridge Design with  $A_s' < A_s$

File: ZWAX.ZWA

### Record of the input

\* Ultimate limit state for bending and longitudinal force EN 1992-1-1

\* The Net - section of compression zone will be used

Material - No.	Strength (N/mm <sup>2</sup> )	E-Modulus (N/mm <sup>2</sup> )	Strain Limits (o/oo)	
			Service	Edge Center
Concrete 1	$f_{c,d} = 23.3$	$E_c = 34100.$	Compres -3.50	-2.00
Reinf.Steel 2	$f_{y,d} = 434.8$	$E_s = 200000.$	Tension 10.00	2.17
Prest.Steel 3	$f_{p,d} = 1304.3$	$E_p = 195000.$		

### Cross-section: Web Cross-Section

Calculation for non-compressive section

Distance between edge and outest tension reinforcement will be calculated

Polygonal Cross-Section 1  
 Concrete (=Material 1)

Coordinates

y (m)	z (m)	Point
0.000	0.000	1
1.200	0.000	2
1.200	0.150	3
0.600	0.300	4
0.400	1.000	5
-0.400	1.000	6
-0.600	0.300	7
-1.200	0.150	8
-1.200	0.000	9

Cross-Section No	Slap	Concrete Mat-No	Point 1 y1 (m)	Point 1 z1 (m)	Dimension Ra=	Dimension Ri=	(m)	Alfa (Degree)
2	Circ.Recess	1	Middle=	0.000	0.500	0.000	0.400	

Point-, Line- and Ring-Reinforcement

No	Slap	Prio	Mat-No.	Cross-Sect. min	Cross-Sect. max	As	Point 1 y1 (m)	Point 1 z1 (m)	Point 2 y2 (m)	Point 2 z2 (m)	reflected
1	Line	-1	2	0.0	100.0	cm2/m	0.000	0.050	1.150	0.050	
2	Line	-1	2	0.0	100.0	cm2/m	-1.150	0.050	0.000	0.050	
3	Line	1	2	0.0	100.0	cm2/m	1.150	0.050	1.150	0.111	
4	Line	1	2	0.0	100.0	cm2/m	1.150	0.111	0.560	0.258	
5	Line	1	2	0.0	100.0	cm2/m	0.560	0.258	0.362	0.950	
6	Line	1	2	0.0	100.0	cm2/m	0.362	0.950	-0.362	0.950	
7	Line	1	2	0.0	100.0	cm2/m	-0.362	0.950	-0.560	0.258	
8	Line	1	2	0.0	100.0	cm2/m	-0.560	0.258	-1.150	0.111	
9	Line	1	2	0.0	100.0	cm2/m	-1.150	0.111	-1.150	0.050	

RIB ZWAX 18.0 Biaxial bending with normal force

Footbridge Design with As' < As

Loc: Midspan

Lc	NEx (kN)	MEy (kNm)	MEz (kNm)
1	0.0	1200.0	400.0

### Cross-section: Web Cross-Section

Calculation for non-compressive section  
 Distance between edge and outest tension reinforcement will be calculated

Polygonal Cross-Section 1  
 Concrete (=Material 1)

Coordinates

y (m)	z (m)	Point
0.000	0.000	1
1.200	0.000	2
1.200	0.150	3
0.600	0.300	4
0.400	1.000	5
-0.400	1.000	6
-0.600	0.300	7
-1.200	0.150	8
-1.200	0.000	9

Cross-Section No	Slap	Concrete Mat-No	Point 1 y1 (m)	z1 (m)	Dimension (m)	Alfa (Degree)
2	Circ.Recess	1	Middle=	0.000	0.500	Ra= 0.000 Ri= 0.400

Point-, Line- and Ring-Reinforcement

No	Slap	Prio	Mat-No.	Cross-Sect. min	max	As	Point 1 y1 (m)	z1 (m)	Point 2 y2 (m)	z2 (m)	reflected
1	Line	-1	2	0.0	100.0	cm2/m	0.000	0.050	1.150	0.050	
2	Line	-1	2	0.0	100.0	cm2/m	-1.150	0.050	0.000	0.050	
3	Line	1	2	0.0	100.0	cm2/m	1.150	0.050	1.150	0.111	
4	Line	1	2	0.0	100.0	cm2/m	1.150	0.111	0.560	0.258	
5	Line	1	2	0.0	100.0	cm2/m	0.560	0.258	0.362	0.950	
6	Line	1	2	0.0	100.0	cm2/m	0.362	0.950	-0.362	0.950	
7	Line	1	2	0.0	100.0	cm2/m	-0.362	0.950	-0.560	0.258	
8	Line	1	2	0.0	100.0	cm2/m	-0.560	0.258	-1.150	0.111	
9	Line	1	2	0.0	100.0	cm2/m	-1.150	0.111	-1.150	0.050	

Loc: Stütze

Lc	NEx (kN)	MEy (kNm)	MEz (kNm)
1	0.0	-2000.0	-600.0

RIB ZWAX 18.0 Biaxial bending with normal force

Footbridge Design with As' < As

## Result

Cross-Section: Web Cross-Section Location: Midspan

Gross Cross-Section I1 = 0.083217 m<sup>4</sup> ys = -0.0000 m  
 A = 0.8273 m<sup>2</sup> Alfa = 0.00 I2 = 0.294361 m<sup>4</sup> zs = 0.3298 m

Reinforcement (R=Priority M=Material)

As No	min.As		max.As (cm <sup>2</sup> )	required.As		Coordinates (m)				Eps.0 o/oo
	R	M		(cm <sup>2</sup> )	cm <sup>2</sup> /m	y1	z1	y2	z2	
3	1	2	0.0	6.1	1.1	17.3	1.150	0.050	1.150	0.111
4	1	2	0.0	60.8	10.5	17.3	1.150	0.111	0.560	0.258
5	1	2	0.0	71.9	12.4	17.3	0.560	0.258	0.362	0.950
6	1	2	0.0	72.5	12.5	17.3	0.362	0.950	-0.362	0.950
7	1	2	0.0	71.9	12.4	17.3	-0.362	0.950	-0.560	0.258
8	1	2	0.0	60.8	10.5	17.3	-0.560	0.258	-1.150	0.111
9	1	2	0.0	6.1	1.1	17.3	-1.150	0.111	-1.150	0.050
Total			0.0	580.1	60.6		required		.As/A_gross = 0.732 %	

Design for Ultimate LS As = 60.6 cm<sup>2</sup>

Lc	Bearing capacity			Strain (o/oo)			Beta Degree	Gamma	Uti- lization
	NRx (kN)	MRy (kNm)	MRz (kNm)	Eps.1	Eps.2	Eps.s			
1	0.	1200.	400.	-1.238	10.583	10.00	0.9	1.000	1.000

Cross-Section: Web Cross-Section Location: Stütze

Gross Cross-Section I1 = 0.083217 m<sup>4</sup> ys = -0.0000 m  
 A = 0.8273 m<sup>2</sup> Alfa = 0.00 I2 = 0.294361 m<sup>4</sup> zs = 0.3298 m

Reinforcement (R=Priority M=Material)

As No	min.As		max.As (cm <sup>2</sup> )	required.As		Coordinates (m)				Eps.0 o/oo
	R	M		(cm <sup>2</sup> )	cm <sup>2</sup> /m	y1	z1	y2	z2	
1	-1	2	0.0	115.0	28.4	24.7	0.000	0.050	1.150	0.050
2	-1	2	0.0	115.0	28.4	24.7	-1.150	0.050	0.000	0.050
Total			0.0	580.1	56.8		required		.As/A_gross = 0.687 %	

---

RIB ZWAX 18.0 Biaxial bending with normal force

Footbridge Design with  $A_s' < A_s$

Design for Ultimate LS  $A_s = 56.8 \text{ cm}^2$

-----

Lc	Bearing capacity			Strain (o/oo)			Beta Gamma Degree	Uti- lization	
	NRx (kN)	MRy (kNm)	MRz (kNm)	Eps.1	Eps.2	Eps.s			
1	0.	-2000.	-600.	-3.152	10.571	10.00	206.7	1.000	1.000

RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Tragfähigkeit

File: ZWAX.ZWA

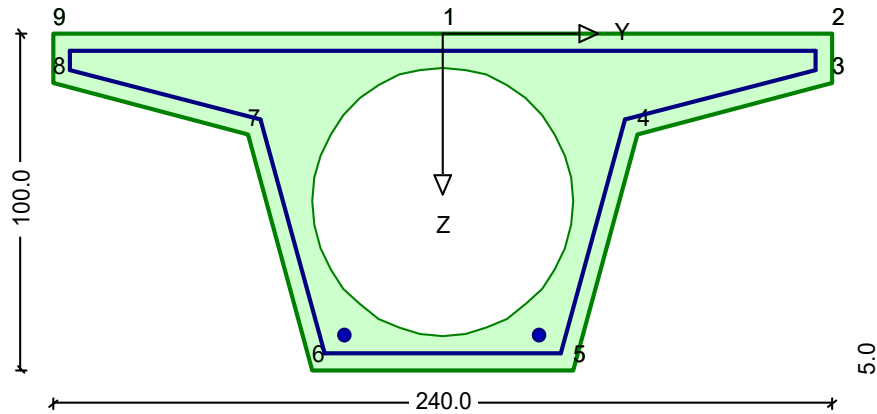
## Echoprint of input data

KOPF Fußgängersteg vorgespannt - Tragfähigkeit  
SEIT 1 1 1 69 1 3  
MATE 19.8333 34100 434.783 1 2 1 1304.35 195000 \*  
-3.5 10 -2 2.381 200000 35  
QUER 'Stegquerschnitt' 0 1  
TQP 1 1 2 0 0 2  
PU 0 0 1  
PU 1.2 0 2  
PU 1.2 0.15 3  
PU 0.6 0.3 4  
PU 0.4 1 5  
PU -0.4 1 6  
PU -0.6 0.3 7  
PU -1.2 0.15 8  
PU -1.2 0 9  
TQR 2 1 2 0 0 0 0.5 0 0.4 0 2  
AS 1 -1 2 0. 0 100 0 0.05 1.15 0.05 0  
AS 2 -1 2 0. 0 100 -1.15 0.05 0 0.05 0  
AS 3 1 2 0. 0 100 1.15 0.05 1.15 0.110961 0  
AS 4 1 2 0. 0 100 1.15 0.110961 0.559857 0.258497 0  
AS 5 1 2 0. 0 100 0.559857 0.258497 0.362285 0.95 0  
AS 6 1 2 0. 0 100 0.362285 0.95 -0.362285 0.95 0  
AS 7 1 2 0. 0 100 -0.362285 0.95 -0.559857 0.258497 0  
AS 8 1 2 0. 0 100 -0.559857 0.258497 -1.15 0.110961 0  
AS 9 1 2 0. 0 100 -1.15 0.110961 -1.15 0.05 0  
AS 10 1 3 3.6 12 12.001 0.3 0.9 - - 2  
ORT 'Feldmitte' 0  
LF 1 0. 2720. 290.  
WAHL 1/8/9  
ENDE

RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Tragfähigkeit

### Record of the input



Bereich: Fußgängersteg vorgespannt - Tragfähigkeit, Querschnitt: Stegquerschnitt

\* Ultimate limit state for bending and longitudinal force EN 1992-1-1

uniaxial bending (neutral axis parallel to y-axis)

\* The Net - section of compression zone will be used

Material - No.	Strength(N/mm <sup>2</sup> )	E-Modulus(N/mm <sup>2</sup> )	Strain Limits(o/oo)	
			Service	Edge Center
Concrete 1	$f_{c.d} = 19.8$	$E.c = 34100.$	Compress	-3.50 -2.00
Reinf.Steel 2	$f_{y.d} = 434.8$	$E.s = 200000.$	Tension	10.00 2.38
Prest.Steel 3	$f_{p.d} = 1304.3$	$E.p = 195000.$		

### Cross-section: Stegquerschnitt

Calculation for non-compressive section

Distance between edge and outest tension reinforcement will be calculated

Polygonal Cross-Section 1  
 Concrete (=Material 1)

Coordinates

y (m)	z (m)	Point
0.000	0.000	1
1.200	0.000	2
1.200	0.150	3
0.600	0.300	4
0.400	1.000	5
-0.400	1.000	6
-0.600	0.300	7
-1.200	0.150	8
-1.200	0.000	9

Cross-Section No	Concrete Slap	Mat-No	Point 1 y1 (m)	z1 (m)	Dimension (m)	Alfa (Degree)
------------------	---------------	--------	----------------	--------	---------------	---------------

2 Circ.Recess      1 Middle=    0.000    0.500 Ra= 0.000 Ri= 0.400

Point-, Line- and Ring-Reinforcement

(Pri=Prio. M=Material      Eps.0=initial strain in prestressing tendon)

No	Slap	Pri	M	Eps.0 (o/oo)	Cross-Sect. As		Point 1		Point 2		refle	
					min	max	y1 (m)	z1 (m)	y2 (m)	z2 (m)	cted	
1	Line	-1	2	0.000	0.0	100.0	cm2/m	0.000	0.050	1.150	0.050	
2	Line	-1	2	0.000	0.0	100.0	cm2/m	-1.150	0.050	0.000	0.050	
3	Line	1	2	0.000	0.0	100.0	cm2/m	1.150	0.050	1.150	0.111	
4	Line	1	2	0.000	0.0	100.0	cm2/m	1.150	0.111	0.560	0.258	
5	Line	1	2	0.000	0.0	100.0	cm2/m	0.560	0.258	0.362	0.950	
6	Line	1	2	0.000	0.0	100.0	cm2/m	0.362	0.950	-0.362	0.950	



RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Tragfähigkeit

No	Slap	Pri	M	Eps.0 (o/oo)	Cross-Sect. min	As max	Point 1 y1 (m)	z1 (m)	Point 2 y2 (m)	z2 (m)	refle cted
7	Line	1	2	0.000	0.0	100.0	cm2/m	-0.362	0.950	-0.560	0.258
8	Line	1	2	0.000	0.0	100.0	cm2/m	-0.560	0.258	-1.150	0.111
9	Line	1	2	0.000	0.0	100.0	cm2/m	-1.150	0.111	-1.150	0.050
10	Point	1	3	3.600	12.0	12.0	cm2	0.300	0.900		at z

Loc: Feldmitte

Lc	NEx (kN)	MEy (kNm)	MEz (kNm)
1	0.0	2720.0	290.0

## Result

Cross-Section: Stegquerschnitt Location: Feldmitte

Gross Cross-Section I1 = 0.083217 m4 ys = -0.0000 m  
 A = 0.8273 m2 Alfa = 0.00 I2 = 0.294361 m4 zs = 0.3298 m

Reinforcement (R=Priority M=Material)

As No	R	M	min.As (cm2)	max.As (cm2)	required.As (cm2)	cm2/m	Coordinates (m)				Eps.0 o/oo
							y1	z1	y2	z2	
3	1	2	0.0	6.1	0.0	0.6	1.150	0.050	1.150	0.111	
4	1	2	0.0	60.8	0.4	0.6	1.150	0.111	0.560	0.258	
5	1	2	0.0	71.9	0.4	0.6	0.560	0.258	0.362	0.950	
6	1	2	0.0	72.5	0.4	0.6	0.362	0.950	-0.362	0.950	
7	1	2	0.0	71.9	0.4	0.6	-0.362	0.950	-0.560	0.258	
8	1	2	0.0	60.8	0.4	0.6	-0.560	0.258	-1.150	0.111	
9	1	2	0.0	6.1	0.0	0.6	-1.150	0.111	-1.150	0.050	
10	1	3	12.0	12.0	12.0		0.300	0.900			3.600
11	1	3	12.0	12.0	12.0		-0.300	0.900			3.600
Total			24.0	604.1	26.1	required					.As/A_gross = 0.315 %

Design for Ultimate LS As = 26.1 cm2

Lc	Bearing capacity			Strain (o/oo)			Beta	Gamma	Uti-
	NRx (kN)	MRy (kNm)	MRz (kNm)	Eps.1	Eps.2	Eps.s	Degree		lization
1	0.	2720.	0.	-1.466	10.603	10.00	0.0	1.000	1.000

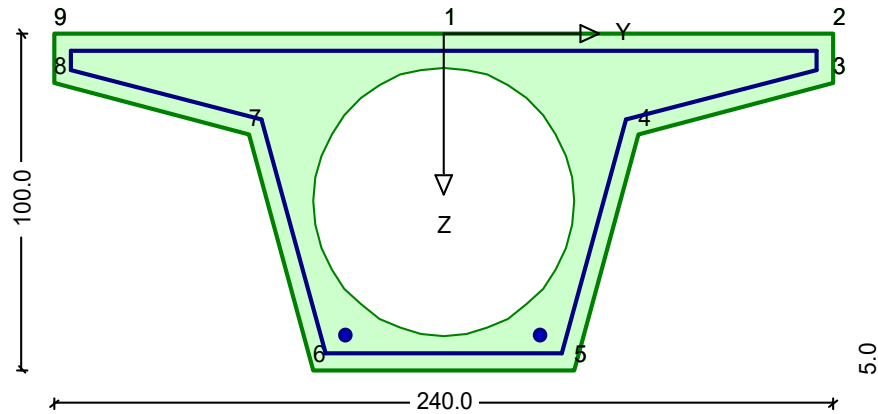
Lc	----Compressive Resultant----				-----Tensile Resultant-----				Lever
	(kN)	y (m)	z (m)	A (m2)	(kN)	y (m)	z (m)	A (m2)	arm (m)
1	-3196.	-0.000	0.044	0.2878	3196.	0.000	0.895	0.00259	0.8510

RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Dehnung

File: ZWAX.ZWA

### Echoprint of input data



Bereich: Fußgängersteg vorgespannt - Dehnung , Querschnitt: Stegquerschnitt

```

KOPF Fußgängersteg vorgespannt - Dehnung
SEIT 1 1 1 69 1 3
MATE 23.3333 34100 434.783 1 2 1 1304.35 195000 *
      -3.5 10 -2 2.17391 200000 35
MATZ 4 1 -10 0 -370 -185 0
QUER 'Stegquerschnitt' 0 1
TQP 1 1 2 0 0 2
PU 0 0 1
PU 1.2 0 2
PU 1.2 0.15 3
PU 0.6 0.3 4
PU 0.4 1 5
PU -0.4 1 6
PU -0.6 0.3 7
PU -1.2 0.15 8
PU -1.2 0 9
TQR 2 1 2 0 0 0 0.5 0 0.4 0 2
AS 1 -1 2 0. 0 100 0 0.05 1.15 0.05 0
AS 2 -1 2 0. 0 100 -1.15 0.05 0 0.05 0
AS 3 1 2 0. 0 100 1.15 0.05 1.15 0.110961 0
AS 4 1 2 0. 0 100 1.15 0.110961 0.559857 0.258497 0
AS 5 1 2 0. 0 100 0.559857 0.258497 0.362285 0.95 0
AS 6 1 2 0. 0 100 0.362285 0.95 -0.362285 0.95 0
AS 7 1 2 0. 0 100 -0.362285 0.95 -0.559857 0.258497 0
AS 8 1 2 0. 0 100 -0.559857 0.258497 -1.15 0.110961 0
AS 9 1 2 0. 0 100 -1.15 0.110961 -1.15 0.05 0
AS 10 1 3 3.6 12 12.001 0.3 0.9 - - 2
ORT 'Feldmitte' 0
LF 1 0. 2720. 290.
WAHL 1/3/8
ENDE
  
```

RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Dehnung

## Record of the input

\* Ultimate limit state for bending and longitudinal force EN 1992-1-1

\* Serviceability limit state for Strain Check under cracked conditions  
 with  $E_c = 34100$ . N/mm<sup>2</sup>. Concrete elastic compression, without tensile strength

\* The Net - section of compression zone will be used

Material - No.	Strength(N/mm <sup>2</sup> )	E-Modulus(N/mm <sup>2</sup> )	Strain Limits(o/oo)	
			Service	Edge Center
Concrete 1	$f_{c,d} = 23.3$	$E_c = 34100$ .	Compress	-3.50 -2.00
Reinf.Steel 2	$f_{y,d} = 434.8$	$E_s = 200000$ .	Tension	10.00 2.17
Prest.Steel 3	$f_{p,d} = 1304.3$	$E_p = 195000$ .		

Additional stress-strain diagrams

Material	Part	Strain(o/oo)		-----Stresses(N/mm <sup>2</sup> )-----		
		Eps.1	Eps.2	Sigma.1	Sigma.m	Sigma.2
4	1	-10.000	0.000	-370.00	-185.00	0.00

## Cross-section: Stegquerschnitt

Calculation for non-compressive section

Distance between edge and outest tension reinforcement will be calculated

Polygonal Cross-Section 1  
 Concrete (=Material 1)

Coordinates

y (m)	z (m)	Point
0.000	0.000	1
1.200	0.000	2
1.200	0.150	3
0.600	0.300	4
0.400	1.000	5
-0.400	1.000	6
-0.600	0.300	7
-1.200	0.150	8
-1.200	0.000	9

Cross-Section No	Concrete Slap	Concrete Mat-No	Point 1		Dimension (m)	Alfa (Degree)
			y1 (m)	z1 (m)		
2	Circ.Recess	1	Middle=	0.000 0.500	Ra= 0.000 Ri= 0.400	

RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Dehnung

Point-, Line- and Ring-Reinforcement

(Pri=Prio. M=Material Eps.0=initial strain in prestressing tendon)

No	Slap	Pri	M	Eps.0 (o/oo)	Cross-Sect. As		Point 1		Point 2		refle	
					min	max	y1 (m)	z1 (m)	y2 (m)	z2 (m)	cted	
1	Line	-1	2	0.000	0.0	100.0	cm2/m	0.000	0.050	1.150	0.050	
2	Line	-1	2	0.000	0.0	100.0	cm2/m	-1.150	0.050	0.000	0.050	
3	Line	1	2	0.000	0.0	100.0	cm2/m	1.150	0.050	1.150	0.111	
4	Line	1	2	0.000	0.0	100.0	cm2/m	1.150	0.111	0.560	0.258	
5	Line	1	2	0.000	0.0	100.0	cm2/m	0.560	0.258	0.362	0.950	
6	Line	1	2	0.000	0.0	100.0	cm2/m	0.362	0.950	-0.362	0.950	
7	Line	1	2	0.000	0.0	100.0	cm2/m	-0.362	0.950	-0.560	0.258	
8	Line	1	2	0.000	0.0	100.0	cm2/m	-0.560	0.258	-1.150	0.111	
9	Line	1	2	0.000	0.0	100.0	cm2/m	-1.150	0.111	-1.150	0.050	
10	Point	1	3	3.600	12.0	12.0	cm2	0.300	0.900			at z

Loc: Feldmitte

Lc	NEx (kN)	MEy (kNm)	MEz (kNm)
1	0.0	2720.0	290.0

## Result

Cross-Section: Stegquerschnitt Location: Feldmitte

Gross Cross-Section I1 = 0.083217 m4 ys = -0.0000 m  
 A = 0.8273 m2 Alfa = 0.00 I2 = 0.294361 m4 zs = 0.3298 m

Reinforcement (R=Priority M=Material)

As No	R	M	min.As (cm2)	max.As (cm2)	required.As (cm2)	cm2/m	Coordinates (m)				Eps.0 o/oo
							y1	z1	y2	z2	
3	1	2	0.0	6.1	0.0	0.4	1.150	0.050	1.150	0.111	
4	1	2	0.0	60.8	0.2	0.4	1.150	0.111	0.560	0.258	
5	1	2	0.0	71.9	0.3	0.4	0.560	0.258	0.362	0.950	
6	1	2	0.0	72.5	0.3	0.4	0.362	0.950	-0.362	0.950	
7	1	2	0.0	71.9	0.3	0.4	-0.362	0.950	-0.560	0.258	
8	1	2	0.0	60.8	0.2	0.4	-0.560	0.258	-1.150	0.111	
9	1	2	0.0	6.1	0.0	0.4	-1.150	0.111	-1.150	0.050	
10	1	3	12.0	12.0	12.0		0.300	0.900			3.600
11	1	3	12.0	12.0	12.0		-0.300	0.900			3.600
Total			24.0	604.1	25.4	required	.As/A_gross = 0.307 %				

RIB ZWAX 18.0 Biaxial bending with normal force

Fußgängersteg vorgespannt - Dehnung

Design for Ultimate LS  $A_s = 25.4 \text{ cm}^2$

Lc	Bearing capacity			Strain (o/oo)			Beta Degree	Gamma	Uti- lization
	NRx (kN)	MRy (kNm)	MRz (kNm)	Eps.1	Eps.2	Eps.s			
1	-0.	2720.	290.	-1.484	10.598	10.00	0.7	1.000	1.000
Lc	----Compressive Resultant----				-----Tensile Resultant-----			Lever	
	(kN)	y (m)	z (m)	A (m2)	(kN)	y (m)	z (m)	A (m2)	arm (m)
1	-3177.	0.091	0.040	0.2640	3177.	-0.000	0.896	0.00253	0.8610

**Check for strain under Service LS  $A_s = 25.4 \text{ cm}^2$   $E_c = 34100.0 \text{ N/mm}^2$**

Lc	Internal stresses SLS			Strain (o/oo)			Beta Deg.	Mue.z (%)	A.ten/ A.gross
	NR (kN)	MRy (kNm)	MRz (kNm)	Eps.1	Eps.2	Eps.s			
1	0.	2720.	290.	-0.735	4.999	4.72	0.6	0.461	0.664
Lc	----Compressive Resultant----				-----Tensile Resultant-----			Lever	
	(kN)	y (m)	z (m)	A (m2)	(kN)	y (m)	z (m)	A (m2)	arm (m)
1	-3169.	0.091	0.039	0.2783	3169.	-0.000	0.898	0.00253	0.8631