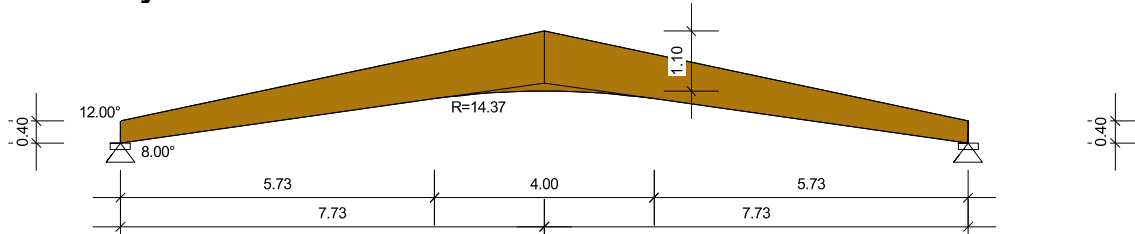


RIB Laminated timber girder (DIN EN 1995-1)

Sattel dach_gekrümmt (DGfH S. 111). RTbsh

Record of the input

Geometry of beam



Beam type	= Saddleback roof symmetric
Beam length	= 15.46 m
Roof slope top	= 12.00 °
Roof slope bottom	= 8.00 °
Radius of curvature	= 14.37 m
Straight length before curvature	= 5.73 m
Width of beam	= 0.16 m
Area	= 10.670 m ²
Volume	= 1.707 m ³
Weight	= 734.09 kg
Length of contour	= 32.19 m
Surface	= 5.150 m ²
Ridge wedge is mounted	

Support conditions

x ... [m] Distance from left end of beam
 dx ... Displacement in x-direction
 dz ... Displacement in z-direction
 rx ... Torsion, x

x [m]	Support type	dx	dz	rx	Notch
0.00	Support left	fixed	fixed	fixed	no
15.46	Support right	free	fixed	fixed	no

Material

E [N/mm ²]	G [N/mm ²]	rho kg/m ³	gamma kN/m ³	f _{m, k} N/mm ²	f _{t, 0, k} N/mm ²	f _{t, 90, k} N/mm ²	f _{c, 0, k} N/mm ²	f _{c, 90, k} N/mm ²	f _{v, k} N/mm ²
13700	850	430.00	5.00	32.00	22.50	0.50	29.00	3.30	2.50

Material name = GL32h
 Thickness of rib = 3.30 cm
 Direction of fibre = Parallel with bottom edge

Building

Height = 12.00 m
 Depth = 20.00 m
 Distance of beam = 1.00 m
 Distance to edge of roof: = 1.50 m
 Elevation of building over NN = 400 m
 Speed pressure q = 0.00 kN/m²
 Characteristic snow load s_k = 5.00 kN/m²

Usage class

UC = 1 ... 20° and 65% rel. Humidity (closed heated buildings)



Cross-section values

x ... [m] Distance from left end of beam
 b ... [cm] Width of cross-section
 h ... [cm] Height of cross-section
 A ... [cm²] Area of cross-section b*h
 I_y ... [cm⁴] Moment of inertia
 W_y ... [cm³] Section modulus
 alfa-t ... Face angle of fibre above
 alfa-b ... Face angle of fibre below

x [m]	b [cm]	h [cm]	A [cm ²]	I _y [cm ⁴]	W _y [cm ³]	alfa-t [°]	alfa-b [°]
0.00	16.00	39.39	630.28	81503	4138	4.00	0.00
7.73	16.00	109.19	1747.03	1735728	31793	12.00	0.00
15.46	16.00	39.39	630.28	81503	4138	4.00	0.00

Safety

Type	Description	gamma-sup	gamma-inf	psi-0	psi-1	psi-2
G	permanent	1.35	1.00	1.00	1.00	1.00
S	Snow	1.50	0.00	0.50	0.20	0.00

Loading

p1 ... [kN/m²] Load value left
 p2 ... [kN/m²] Load value right
 x1 ... [m] Load position left
 x2 ... [m] Load position right

Load case Ständige Last (Permanent load)

Type	p1	p2	x1	x2
Line load	3.60	3.60	0.00	7.73
Line load	3.60	3.60	7.73	15.46

Load case Snow entire roof (Snow)

Type	p1	p2	x1	x2
Line load	4.00	4.00	0.00	7.73
Line load	4.00	4.00	7.73	15.46

Load case Snow left (Snow)

Type	p1	p2	x1	x2
Line load	4.00	4.00	0.00	7.73
Line load	2.00	2.00	7.73	15.46

Load case Snow right (Snow)

Type	p1	p2	x1	x2
Line load	2.00	2.00	0.00	7.73
Line load	4.00	4.00	7.73	15.46

Results

Summary of utilization

	x	actual /perm
ULS:	3.23	1.03*
Bending stress:	3.23	1.03*
Shear stress:	14.88	0.96
Support pressure:	0.00	0.44
SLS:	7.73	1.44*
w, inst:	7.73	1.44*
w, fin sel dom:	7.73	1.23*
w, fin qu. st. - w0:	7.73	0.73
Fire protection avail/allow		
ULS:	7.73	0.52
Bending stress:	3.23	0.43
Shear stress:	14.88	0.39

Characteristic support values

x [m]	Type	Ax, min [kN]	Ax, max [kN]	Az, min [kN]	Az, max [kN]
0.00	G	0.00	0.00	28.41	28.41
15.46	G	0.00	0.00	28.41	28.41
0.00	S	0.00	0.00	0.00	30.92
15.46	S	0.00	0.00	0.00	30.92
0.00	Sum	0.00	0.00	28.41	59.33
15.46	Sum	0.00	0.00	28.41	59.33

Characteristic deflections

Filel	x [m]	w-min [mm]	x [m]	w-max [mm]
1	0.00	0.00	7.73	74.06

Transverse tension

Transverse tensile stress

sig_{t90} ... Transverse tension stress GI (6.54)
 eta ... Utilization transverse tension stress GI (6.53)
 eta-lim ... <= 1 -> in UC 1+2 no constc. Bracing necessary
 My_d ... Design moment at crest point
 sig_{-ul} ... Longitudinal stress at bottom of ridge section GL (6.42)
 eta ... Utilization longitudinal stress of ridge section GI (6.41)

x [m]	sig _{t90} [N/mm ²]	eta	eta-lim	My _d [kNm]	sig _{-ul} [N/mm ²]	eta	kmod
7.73	0.49	4.77	7.95	327.3	14.96	0.68	0.90

Bracing of transverse tension

Full threaded bolts (SPAX Z-9.1-519)

allow. distance at UE > 25.0 cm and < 82.3 cm
 Tensile strength steel f_{t,d} = 1.00 N/mm²

x_a, x_e ... area to reinforce, outer and inner quarter
 d ... Diameter of steel
 n ... Total number of bars in the domain
 n_l ... Number of bars in longitudinal direction
 n_q ... Number of bars in normal direction
 a₁ ... distance of bar at top edge of beam's length
 a₂ ... Minimum distance together cross
 a_{2c} ... Minimum distance to cross edge

 Rax, d ... Capacity of tensile force due to extraction

Ft90, d ... Design tension force

lad ... Effective length of anchorage

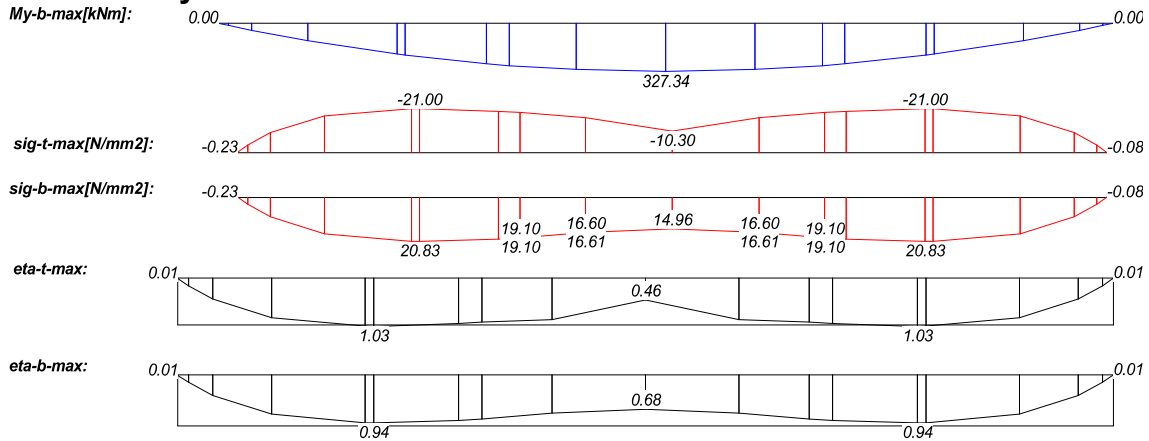
eta ... Utilisation from extraction

eta-St ... Utilisation of tensile strength

n = -1: not allowable

xam	xem	dmm	n	nl	nq	a1cm	a2cm	a2ccm	Rax, dkN	Ft90, dkN	ladcm	eta	eta-St
5.73	6.73	8	4	4	1	27.0	2.0	3.2	17.1	13.4	39.8	0.78	0.99
6.73	8.73	8	12	6	2	35.2	2.0	3.2	19.5	13.4	45.5	0.69	0.99
8.73	9.73	8	4	4	1	27.0	2.0	3.2	17.1	13.4	39.8	0.78	0.99
5.73	6.73	10	3	3	1	36.0	2.5	4.0	21.4	17.9	39.8	0.84	0.80
6.73	8.73	10	8	8	1	26.4	2.5	4.0	24.4	20.1	45.5	0.82	0.90
8.73	9.73	10	3	3	1	36.0	2.5	4.0	21.4	17.9	39.8	0.84	0.80
5.73	6.73	12	3	3	1	36.0	3.0	4.8	25.6	17.9	39.8	0.70	0.59
6.73	8.73	12	6	6	1	35.2	3.0	4.8	29.3	26.8	45.5	0.92	0.88
8.73	9.73	12	3	3	1	36.0	3.0	4.8	25.6	17.9	39.8	0.70	0.59

Stress analysis



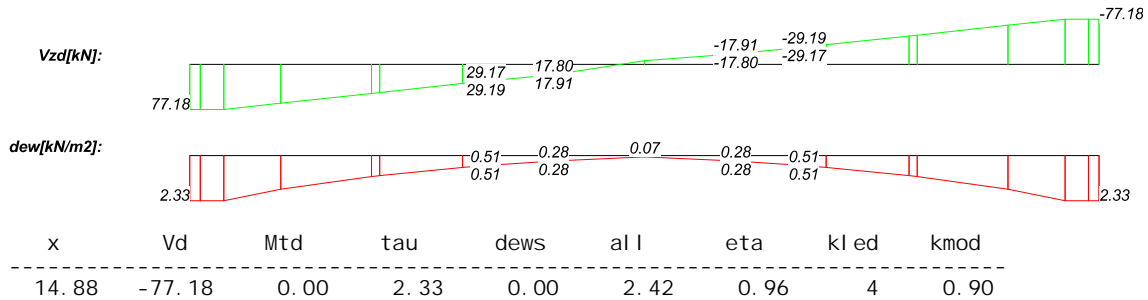
maximum longitudinal stress

Myd ... [kNm] Design moment
 sig ... [N/mm2] Bending stress
 allsig ... [N/mm2] permissible shear stress
 eta ... Utilisation level
 kmod ... Modification coefficient
 kled ... Duration of loads

kled=1 ..permanent, 2 ... long, 3 ... mid, 4 ... short, 5 ... very short

x	Myd	sig, o	allsig	eta-0	kled	kmod	sig, u	allsig	eta-b	kled	kmod
3.23	216.58	-21.00	20.35	1.03*	4	0.90	20.83	22.06	0.94	4	0.90
7.73	327.34	-10.30	22.15	0.46	4	0.90	14.96	22.15	0.68	4	0.90
12.23	216.58	-21.00	20.35	1.03*	4	0.90	20.83	22.06	0.94	4	0.90

Shear stresses



Support pressure and safety

Avd ... [kN] Design value of support reaction
 alfa ... [°] Angle between force and fibre direction
 kc90 ... Coefficient of transverse compression

x	Avd-min	Avd-max	kled	kmod	alfa	kc90	Width	sig-alf	all	eta
0.00	28.41	84.74	4	0.90	82.00	1.75	0.36	1.36	3.08	0.44
15.46	28.41	84.74	4	0.90	82.00	1.75	0.36	1.36	3.08	0.44

Check of deflections

wG,inst ... Initial deformation due to permanent loads
 wG,fin ... End deformation due to permanent load
 wQ,inst.s ... Initial deformation due to variable loads (rare combination)
 wQ,fin.s ... End deformation due to variable loads (rare combination)
 wQ,inst.q ... Initial deformation due to variable loads (quasi-permanent combination)
 wQ,fin.q ... End deformation due to variable loads (Quasi-permanent combination)
 w0 = 0.0 mm ... [mm] given camber
 L' ... [m] Length of span
 all ... [mm] allowance deflection
 L'/w ... relationship between length and deflection
 w,inst ... elastic initial deflection under rare action combination
 w,inst = wG,inst + wQ,inst.s
 w,fin.s ... Total deflection under rare action combination
 w,fin.s = w,fin(G+Q).s
 w,fin.q ... Total deflection under quasi-permanent action combination
 w,fin.q = w,fin(G+Q).q - w0
 Camber is already subtracted from deflection wfin.q of main span.

Minimal:

Fiel	L'	x	w,inst	all	L'/w	x	wfin.s	all	L'/w	x	wfin.q	all	L'/w
1	15.46	0.00	0.0	51.5	-	0.00	0.0	77.3	-	0.00	0.0	77.3	-

Maximum:

Fiel	L'	x	w,inst	all	L'/w	x	wfin.s	all	L'/w	x	wfin.q	all	L'/w
1	15.46	7.73	74.1	51.5	209	7.73	95.3	77.3	162	7.73	56.7	77.3	273

Results of load case fire

Burnout ... Tri lateral
Fire resistance class ... F 30 -B

Remaining cross-section

d(tf) ... [cm] Depth of combustion
Ar ... [cm²] Area
Wr ... [cm³] Section modulus
ur ... [cm] Flamed Circumference
k, fi ... Modification coefficient of stiffness (Tab. 75)
kmod, m, fi ... Modification coefficient of bending strength
kmod, E, fi ... Modification coefficient of stiffness

x [m]	d(tf) [cm]	ur [cm]	Ar [cm ²]	Wr [cm ³]	k, fi	kmod, m, fi	kmod, E, fi
0.00	2.80	83.58	380.56	2320.93	1.15	1.00	1.00
0.18	2.80	86.14	393.84	2485.69	1.15	1.00	1.00
0.58	2.80	91.81	423.34	2872.06	1.15	1.00	1.00
1.55	2.80	105.51	494.59	3920.19	1.15	1.00	1.00
3.09	2.80	127.44	608.62	5936.22	1.15	1.00	1.00
3.23	2.80	129.43	618.95	6139.37	1.15	1.00	1.00
4.64	2.80	149.37	722.65	8369.01	1.15	1.00	1.00
5.03	2.80	154.85	751.16	9042.32	1.15	1.00	1.00
6.18	2.80	173.20	846.56	11484.87	1.15	1.00	1.00
7.73	2.80	223.18	1106.45	19619.13	1.15	1.00	1.00
9.28	2.80	173.20	846.56	11484.87	1.15	1.00	1.00
10.44	2.80	154.85	751.16	9042.32	1.15	1.00	1.00
10.82	2.80	149.37	722.65	8369.01	1.15	1.00	1.00
12.23	2.80	129.43	618.95	6139.37	1.15	1.00	1.00
12.37	2.80	127.44	608.62	5936.22	1.15	1.00	1.00
13.91	2.80	105.51	494.59	3920.19	1.15	1.00	1.00
14.88	2.80	91.81	423.34	2872.06	1.15	1.00	1.00
15.28	2.80	86.14	393.84	2485.69	1.15	1.00	1.00
15.46	2.80	83.58	380.56	2320.93	1.15	1.00	1.00

Transverse tensile in case of fire

Transverse tensile stress in case of fire

x [m]	sig _{t90} [N/mm ²]	eta	eta-lim	My _d [kNm]	sig _{ul} [N/mm ²]	eta	kmod
7.73	0.32	0.52	3.16	133.6	9.90	0.27	0.90

Bracing of transverse tensile in case of fire

Full threaded bolts (SPAX Z-9.1-519)

allow. distance at UE > 25.0 cm and < 82.3 cm

Tensile strength steel $f_t, d = 1.00$ N/mm²

n = -1: not allowable

x _a m	x _e m	d mm	n	n _l	n _q	a ₁ cm	a ₂ cm	a _{2c} cm	R _{ax, d} kN	F _{t90, d} kN	l _{ad} cm	eta	eta-St
5.73	6.73	8	2	2	1	54.0	0.0	0.0	22.2	0.0	39.8	0.00	0.00
6.73	8.73	8	3	3	1	70.4	0.0	0.0	22.2	0.0	39.8	0.00	0.00
8.73	9.73	8	2	2	1	54.0	0.0	0.0	22.2	0.0	39.8	0.00	0.00
5.73	6.73	10	2	2	1	54.0	0.0	0.0	27.8	0.0	39.8	0.00	0.00
6.73	8.73	10	3	3	1	70.4	0.0	0.0	27.8	0.0	39.8	0.00	0.00
8.73	9.73	10	2	2	1	54.0	0.0	0.0	27.8	0.0	39.8	0.00	0.00
5.73	6.73	12	2	2	1	54.0	0.0	0.0	33.3	0.0	39.8	0.00	0.00
6.73	8.73	12	3	3	1	70.4	0.0	0.0	33.3	0.0	39.8	0.00	0.00
8.73	9.73	12	2	2	1	54.0	0.0	0.0	33.3	0.0	39.8	0.00	0.00

Stress analysis

maximum longitudinal stress in case of fire

x	Myd	sig, o	all Sig	eta-0	kled	kmod	sig, u	all sig	eta-b	kled	kmod
3.09	85.55	-14.47	33.87	0.43	4	0.90	14.35	36.74	0.39	4	0.90
7.73	133.59	-6.81	36.80	0.19	4	0.90	9.90	36.80	0.27	4	0.90
12.37	85.55	-14.47	33.87	0.43	4	0.90	14.35	36.74	0.39	4	0.90

Shear stresses in case of fire

x	Vd	Mtd	tau	dews	all	eta	kled	kmod
14.88	-31.51	0.00	1.56	0.00	4.03	0.39	4	0.90